

**Amendments to the Specification:**

Please replace the Abstract with the attached amended Abstract.

Please replace the paragraph beginning on page 5, line 18, with the following rewritten paragraph:

When  $f_{1-2}/f_3$  is greater than -1.5 and smaller ~~than -0.8~~, i.e., when  $f_{1-2}/f_3$  is in the vicinity of -1, light rays traveling from the side of the screen and falling on the first lens substantially parallel to the optical axis emerge from the third lens substantially parallel to the optical axis and fall in substantially parallel light rays on the fourth lens. Light rays traveling from the side of the screen and fallen on the first lens obliquely to the optical axis emerge from the third lens and fall on the fourth lens without greatly changing the traveling direction. Thus, the set of the first and the second lens, and the third lens form the so-called afocal lens system, which reduces aberration attributable to the projection lens. When  $f_{1-2}/f_3$  is -1.5 or below or -0.8 or above, light rays traveling from the side of the screen and fallen on the first lens substantially parallel to the optical axis fall obliquely on the fourth lens. Consequently, load for reducing aberration on the fourth lens increases, and the projection lens is liable to cause aberrations.

Please replace the paragraph beginning on page 12, line 6, with the following rewritten paragraph:

The value of  $f_{1-2}/f_3$  must be within such a range defined by Expression (3) for the following reasons. When  $f_{1-2}/f_3$  is greater than -1.5 and smaller ~~than -0.8~~, i.e., when  $f_{1-2}/f_3$  is in the vicinity of -1, the synthetic power of the first lens 10 and the second lens 20 is approximately equal to the power of the third lens 30, and the synthetic power of the first lens 10 and the second lens 20 and the power of the third lens 30 have opposite signs, respectively. For example, light rays traveling from the side of the screen 5 and falling on the first lens 10 substantially parallel to the optical axis emerge from the third lens substantially parallel to the

optical axis and fall in substantially parallel light rays on the fourth lens 40. Light rays traveling from the side of the screen 5 and fallen on the first lens 10 obliquely to the optical axis emerge from the third lens 30 and fall on the fourth lens 40 without greatly changing the traveling direction. Thus, the set of the first lens 10 and the second lens 20, and the third lens 30 form the so-called afocal lens system, which reduces aberration attributable to the projection lens 2 satisfactorily for the comparatively small number of the constituent lenses. When  $f_{1-2}/f_3$  is -1.5 or below or -0.8 or above, the set of the first lens 10 and the second lens 20, and the third lens 30 are unable to form an afocal lens system and, consequently, light rays traveling from the side of the screen 5 and fallen on the first lens 10 substantially parallel to the optical axis fall obliquely on the fourth lens 40. Consequently, load for aberration correction on the fourth lens 40 increases, and the projection lens 2 is liable to cause aberration. Thus, the first lens 10, the second lens 20 and the third lens 30 of the projection lens 2 have refracting powers to make light rays coming from the side of the screen 5 and falling on the first lens 10 substantially parallel to the optical axis emerge from the third lens 30 substantially parallel to the optical axis.

Please replace the paragraph beginning on page 13, line 21, with the following rewritten paragraph:

Fig. 2 shows data on the projection lens 2 in an example, in which OBJ Nos. are plane numbers of surfaces of the lenses from the side of a screen toward the side of a display device. For example, the number of the aspherical surface 11 of the first lens 10 is OBJ No. 2, and the first lens 10 has lens surfaces OBJ Nos. 1 and 2. The number of the diaphragm 22 is OBJ No. 5. The numbers of the lens surfaces of the second lens 20 are OBJ Nos. 3 and 4. The numbers of the lens surfaces of the third lens 30 are OBJ Nos. 6 and 7. The numbers of the lens surfaces of the fourth lens 40, i.e., a compound lens, are OBJ Nos. 8, 9 and 10. The numbers of the lens surfaces of the fifth lens 50 are OBJ Nos. 11 and 12. The numbers of the

lens surfaces of the sixth lens 60 are OBJ Nos. 13 and 14. RDYs are radii of curvature in millimeter, and THIs are thicknesses of lenses or air spaces. For example, a THI of 2.0 corresponding to OBJ No. 1 is the thickness of the first lens 10, a THI of 27.7 corresponding to OBJ No. 2 is the distance between the back end, on the side of the display device 70 of the first lens 10, and the front end, on the side of the screen 5, of the second lens 20. In Fig. 2, GLA indicated the D line refractive index and the Abbe's number of a material forming the lens. For example a GLA of 1.51680-64.2 indicates a material having a D line refractive index of 1.51680 and an Abbe's number of 64.2.